

**Example 6.4**

In a certain settler, solid-liquid separation is satisfactory when operated under the following conditions:  $X_t = 5 \text{ g}\cdot\text{l}^{-1}$ , superficial loading rate  $T_s = 0.5 \text{ m}\cdot\text{h}^{-1}$  and recycle factor  $s = 1$ . When the superficial loading rate is increased to  $0.55 \text{ m}\cdot\text{h}^{-1}$  the settler fails, independent of the value of the applied recycle factor. The values of the Vesilind constants have been determined as  $k = 0.4 \text{ l}\cdot\text{g}^{-1}$  and  $v_0 = 7 \text{ m}\cdot\text{h}^{-1}$ . Estimate the safety factor of the settler.

**Solution:**

For the data given  $k \cdot X_t = 0.4 \cdot 5 = 2$ . The largest ratio of  $T_s/v_0$  that can be applied for  $T_s = 0.5 \text{ m}\cdot\text{h}^{-1}$  and  $v_0 = 7 \text{ m}\cdot\text{h}^{-1} = T_s/v_0 = 0.5/7 = 0.07$ .

Using Fig. 6.8, point A is identified as the intersection of the curve for  $s=1$  with  $k \cdot X_t = 2$ . The value of the ratio  $T_{sm}/v_0$  for an ideal settler ( $s_f = 1$ ) would be 0.135.  $T_{sm}$  is  $7 \cdot 0.135 = 0.94 \text{ m}\cdot\text{h}^{-1}$ . As the applied  $T_{sm}$  in reality is  $0.5 \text{ m}\cdot\text{h}^{-1}$  the value of the safety factor can be calculated as  $s_f = T_{sm}/T_s = 0.94/0.5 = 1.88 \approx 2$ .

**Example 6.5:**

In the above example, when the concentration  $X_t = 5 \text{ g}\cdot\text{l}^{-1}$  is maintained and the superficial loading rate  $T_s$  is lowered to  $0.25 \text{ m}\cdot\text{h}^{-1}$ , what will be the minimum value of the sludge recycle rate  $s$ ? If a superficial loading rate  $T_s$  of  $0.25 \text{ m}\cdot\text{h}^{-1}$  is applied, what will be the maximum possible concentration  $X_t$  and what will be the required minimum value of sludge recycle factor  $s$ ?

**Solution:**

$k \cdot X_t$  remains 2 and the value of  $T_s/v_0 = 0.25/7 = 0.036$ . Again using Fig. 6.8 and applying the safety factor of 2, then point B is identified. It can be seen that the corresponding  $s$  curve (going through B) is marginally higher than that for  $s = 0.5$ .

As for the second part of the question: when clarification is limiting, for  $s_f = 2$  and  $T_s/v_0 = 0.25/7 = 0.035$  in Fig. 6.8 the corresponding value of  $k \cdot X_t$  can be determined as 2.67 or  $X_t = 2.67/0.4 = 6.7 \text{ g}\cdot\text{l}^{-1}$  (point C). The required recycle rate is determined as  $s = 2$ . For lower values of the sludge recycle factor  $s$ , clarification ceases to be the limiting process. For thickening the required area will be larger.